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High-sensitivity, high-speed, broadband midinfrared photodetector enabled by a van der Waals heterostructure with a vertical transport channel

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The realization of room-temperature-operated, high-performance, miniaturized, low-power-consumption and Complementary Metal-Oxide-Semiconductor (CMOS)-compatible mid-infrared photodetectors is highly desirable for nextgeneration optoelectronic applications, but has thus far remained an outstanding challenge using conventional materials. Two-dimensional (2D) heterostructures provide an alternative path toward this goal, yet despite continued efforts, their performance has not matched that of low-temperature HgCdTe photodetectors. Here, we push the detectivity and response speed of a 2D heterostructure-based mid-infrared photodetector to be comparable to, and even superior to, commercial cooled HgCdTe photodetectors by utilizing a vertical transport channel (graphene/black phosphorus/molybdenum disulfide/ graphene). The minimized carrier transit path of tens of nanometers facilitates efficient and fast carrier transport, leading to significantly improved performance, with a mid-infrared detectivity reaching 2.38×10^{11} cmHz^{1/2}W⁻¹ (approaching the theoretical limit), a fast response time of 10.4 ns at 1550 nm, and an ultrabroadband detection range spanning from the ultraviolet to midinfrared wavelengths. Our study provides design guidelines for next-generation high-performance room-temperature-operated mid-infrared photodetectors.

Mid-infrared photodetection has long been central to various technological applications, including military and defense, environmental monitoring, astronomy, and astrophysics^{1,2}. At the same time, with the emergence of new frontiers such as autonomous driving^{3,4}, smart cities⁵, artificial intelligence⁶, and others, there are greater demands for mid-infrared photodetectors in terms of high sensitivity, high speed, miniaturization, low power consumption, and integration. However, developments in this field using conventional semiconductors such as

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II-IV HgCdTe^{7,8} and III-V superlattices^{9,10} are greatly limited by the requirements for low-temperature cooling operation, bulky module size, high power consumption, complex fabrication processes, and limited compatibility with Complementary Metal-Oxide-Semiconductor (CMOS) technology. Two-dimensional (2D) van der Waals heterostructures are promising for reducing the dark current and achieving high-performance room-temperature-operated midinfrared photodetectors¹¹⁻¹⁷. However, despite continued advancements, simultaneously achieving high sensitivity, fast response speed, and ultrabroadband mid-infrared photodetection remains a persistent challenge.

The first problem is posed by the specific detectivity (D). For a photodetector operated in photovoltaic mode, there exists a theoretical limit for the detectivity, which is known as the background-limited infrared photodetector (BLIP) limit¹⁸:

$$D_{BLIP}^* = \frac{\lambda}{hc} \left(\frac{\eta}{2\Phi_B} \right)^{1/2} \tag{1}$$

where Φ_B is the total background photon flux density reaching the photodetector. Such ideal mid-infrared photodetectors have, however, rarely been experimentally realized. This is primarily attributed to the challenge of achieving devices with extremely low dark noise current and high external quantum efficiency, which is particularly difficult for mid-infrared materials with narrow bandgaps^{11,19-21}. A second problem relates to the limited response speed²². The reported fastest response time of a 2D heterostructure-based mid-infrared photodetector is on the order of microseconds, which is more than two orders of magnitude slower than that of commercial HgCdTe photodetectors^{11,12,15}. An often overlooked issue in response time optimization is the carrier transit time²³, which may extend to microseconds or even longer for photovoltaic devices with low carrier mobility and long channel lengths. To further push the detectivity and response speed to their theoretical limits, an approach that can synergistically reduce the noise current, enhance the external quantum efficiency, and shorten the carrier transit time is highly needed.

Here, we demonstrate the construction of a room-temperatureoperated, self-powered, high-sensitivity, high-speed, and ultrabroadband mid-infrared photodetector utilizing graphene/black phosphorus/molybdenum disulfide/graphene (Gr/BP/MoS₂/Gr) heterostructures with a vertical transport channel. The embedded BP/ MoS₂ p-n junction effectively reduces the room temperature noise current. The minimized vertical channel length of tens of nanometers prevents recombination-induced charge carrier losses during transport, leading to a high external quantum efficiency. Moreover, the shortened transit path results in a substantial reduction in the carrier transit time, overcoming potential limitations on response speed that may otherwise be imposed by an extended carrier transit time. As a result, the fabricated vertical channel device exhibits a roomtemperature mid-infrared detectivity reaching up to 2.38 × 1011 cmHz^{1/2}W⁻¹, approaching the BLIP limit; a fast response time of 10.4 ns at 1550 nm, reaching or even surpassing the response speed of commercial cooled HgCdTe photodetectors in mid-infrared wavelength range; and an ultra-broadband photodetection range spanning ultraviolet, visible, near-infrared and mid-infrared wavelengths. Our findings represent an essential step toward the realization of nextgeneration high-performance, low-power-consumption, and CMOScompatible mid-infrared photodetectors.

Results

Design and optimization of the photodetector structure

Figure 1a illustrates the design concept of the vertical photodetector, and its advantages can be manifested in the following aspects: (i) Vertical transport channel. The steady-state spatial distribution of the

photogenerated excess charge carrier concentration is presented in Fig. 1b. Assuming the generation of photoexcited excess charge carriers at the pn junction without external bias, the carrier concentration undergoes an exponential decay with increasing distance from the junction (Supplementary Note 1 and Supplementary Fig. 1). In 2D material-based photodetectors featuring lateral transport channels. photogenerated charge carriers must diffuse over distances typically on the order of tens of micrometers before reaching the electrodes, resulting in a significant loss of carrier concentration due to recombination. For instance, in a material with a carrier diffusion length of 500 nm, the excess carrier concentration drops from 100% at the junction region to approximately 13.53% and 2.06×10^{-9} at distances of 1 μm and 10 μm from the junction, respectively, leading to a substantial reduction in the external quantum efficiency. The implementation of a vertical channel reduces the transit path length of charge carriers to tens of nanometers, enabling highly efficient carrier transport and, consequently, achieving high quantum efficiency and shorter transit time. (ii) Graphene electrodes. The use of transparent graphene electrodes enables spatial overlap of the junction region with the electrodes, establishing a vertical channel without impeding the transmission of incident light. Leveraging the high carrier mobility of graphene ensures swift extraction of charge carriers to the external circuit, resulting in both high quantum efficiency and rapid response time. Furthermore, encapsulating the BP/MoS₂ heterojunction between two parallel graphene layers serves as a protective measure, mitigating the common issue of ambient degradation in BP-based devices. (iii) BP/MoS₂ heterojunction. At the interface of BP and MoS₂, a type II energy level alignment is established (Fig. 1c, d), which enables the photodetector to operate in photovoltaic mode with remarkably low levels of dark noise current and minimal power consumption. The uniform built-in electric field is precisely oriented along the vertical transit path, ensuring the efficient separation and rapid extraction of photogenerated charge carriers toward the top and bottom electrodes. Furthermore, the synergistic combination of the narrow-gap material BP (0.3 eV) and the wide-gap material MoS₂ (1.2 eV) as absorbers enhances the broadband detection capability of our device. (iv) Au electrodes. The finger electrodes located on the top and the Au pad on the bottom play a crucial role in facilitating the extraction of charge carriers to the external circuit. In addition, the bottom Au pad also serves as a back reflector to amplify the absorption of incident light. Our vertical design allows simultaneous optimization of the response speed, external quantum efficiency, noise current, and detection range, thereby enhancing the overall performance of the photodetector.

Optoelectronic characterization of vertical channel device

Figure 2a, b shows the schematic structure and optical image of the Gr/ BP/MoS₂/Gr vertical channel photodetector. The detailed fabrication procedures are described in the methods section. The exfoliation and transfer processes were conducted in an argon-purged glovebox to prevent BP from oxidation, as confirmed by the Micro-area XPS measurement (Supplementary Fig. 2). The device consists of a BP/MoS₂ heterojunction sandwiched between two graphene layers. Atomic force microscopy (AFM) revealed that the thicknesses of the BP and MoS₂ layers were 27 nm and 14 nm, respectively (Supplementary Fig. 3). High-resolution transmission electron microscopy (HRTEM) and selected area electron diffraction (SAED) measurements confirm the high crystallinity of both BP and MoS₂ (Supplementary Fig. 4). Energy-dispersive X-ray spectroscopy (EDX) mapping and crosssectional HRTEM image reveal the formation of a high-quality heterostructure interface (Supplementary Fig. 5). The transfer characteristics of BP and MoS₂ field-effect transistors exhibit typical p-type and n-type behaviors at zero gate voltage (Supplementary Fig. 6). The Raman spectra measured in the overlapped junction region consist of peaks corresponding to individual BP and MoS₂ layers with negligible

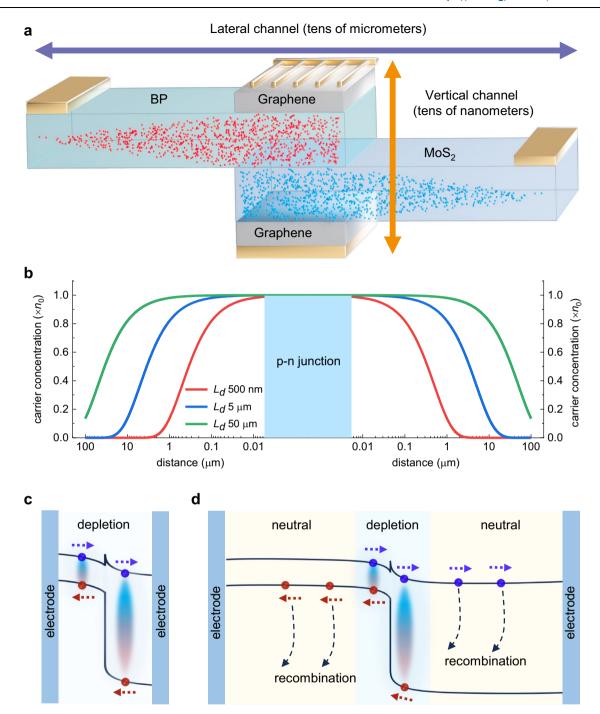


Fig. 1 | **Photogenerated charge carrier transport in 2D heterostructures with vertical and lateral transport channels. a** Schematic diagram illustrating the diffusion process of photogenerated charge carriers in both vertical and lateral channel devices, with incident light directed from above onto the overlapped heterojunction region. The red and blue spheres represent holes and electrons, respectively. **b** Steady-state photogenerated charge carrier distribution as a function of distance from the p-n junction when excess electrons and holes are exclusively generated at the p-n junction region. L_d represents the diffusion length of the

charge carriers. n_0 refers to the photogenerated carrier concentration at the p-n junction region. \mathbf{c} , \mathbf{d} Schematic energy band diagram showing the electron-hole pair generation, separation, diffusion, and recombination processes in both vertical (\mathbf{c}) and lateral channel devices (\mathbf{d}) . The red and blue dashed arrows indicate the transport directions of photogenerated holes and electrons, respectively. The blue and orange shaded areas correspond to the depletion and neutral regions, respectively.

peak shifts¹² (Supplementary Fig. 7), indicating the formation of a high-quality, strain-free vdW heterostructure. To elucidate the underlying working mechanism of this vertical photodetector, we performed scanning photocurrent measurements with a confocal optical microscope at $V_{\rm ds} = 0$ V under the illumination of a 633 nm laser. The scanning photocurrent image, as shown in the inset of Fig. 2b, clearly illustrates that the photocurrent is exclusively generated within the BP/

 MoS_2 overlapping region, delineated by the white dotted line. This indicates that the built-in electric field formed at the p-n junction dominates the separation of the charge carrier and, consequently, the generation of a photocurrent.

Figure 2c shows the I-V characteristics of the vertical device in the dark and under 1550 nm laser excitation at different light powers. Notably, both the open-circuit voltage ($V_{\rm oc}$) and short-circuit current

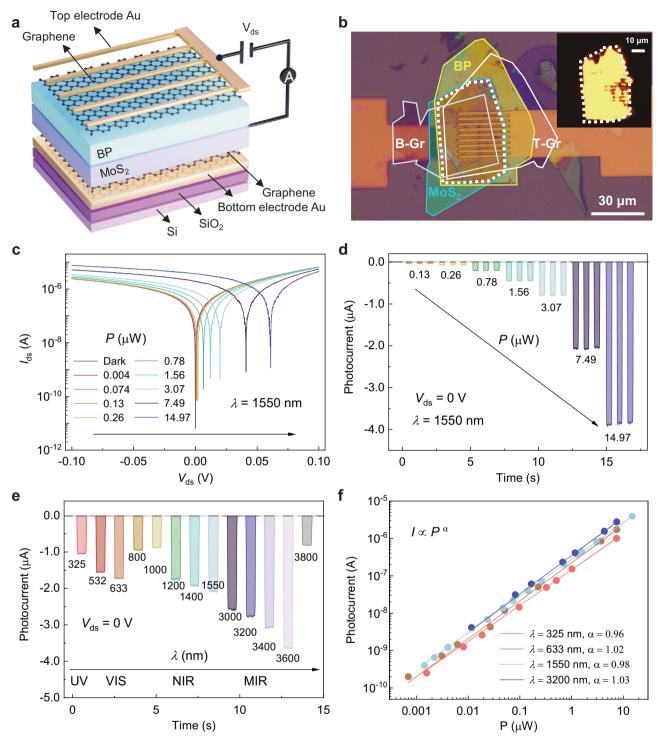


Fig. 2 | **Optoelectronic characterization of the vertical channel photodetector.** a Schematic illustrating the experimental setup of the Gr/BP/MoS₂/Gr vertical channel photodetector. The photocurrent was measured through the top and bottom Au electrodes. A high-resistivity silicon substrate is used to avoid the parasitic capacitance effects caused by the heavily doped silicon substrate. Here, BP and Gr represent black phosphorus and graphene, respectively. V_{ds} indicate the bias applied between the source and drain. **b** Optical image of the fabricated vertical device, with the BP, MoS₂, and graphene layers outlined by yellow, blue, and white lines, respectively, for clarity. Inset: Photocurrent map of the device obtained by scanning a focused laser beam with a wavelength of 633 nm and V_{ds} = 0 V. The area enclosed by the dotted line represents the overlapping region of

the BP/MoS $_2$ heterojunction. **c** Output characteristics of the vertical photodetector in the dark and under 1550 nm laser illumination at different light powers. **d** Timeresolved photoresponse at different light powers at a wavelength of 1550 nm with $V_{\rm ds} = 0$ V. **e** Wavelength-dependent time-resolved photoresponse measured at $V_{\rm ds} = 0$ V with an incident light power of 7.5 μ W. **f** Power dependence of the photocurrent extracted at $V_{\rm ds} = 0$ V for four characteristic spectral bands, namely, the ultraviolet (325 nm), visible (633 nm), near-infrared (1550 nm), and mid-infrared (3200 nm) bands. Here, the dots represent the experiment data, and the lines are the result of fitting the data to a power function. α is an exponent of the power function.

 (I_{sc}) increase with increasing light power and do not saturate within the investigated power range. To further explore the power-dependent photoresponse in self-powered mode, we measured the time-resolved photoresponse at zero bias under various light powers with a 1550 nm. laser. As shown in Fig. 2d, the photocurrent gradually increases with increasing incident light power from 132 nW to 14.97 uW. A sharp increase or decrease in the photocurrent is observed upon switching the incident light on or off, indicating the rapid response of the device. Similar output characteristics and time-resolved photocurrent responses have also been observed for visible and mid-infrared light sources (Supplementary Figs. 8, 9). The wavelength-dependent temporal photoresponse measured at zero bias with an incident light power of 7.5 µW is presented in Fig. 2e, revealing an ultra-broadband photodetection capability spanning from 325 nm to 3800 nm. This extensive range covers wavelengths from the ultraviolet to the visible region and extends into the short-wavelength infrared (SWIR) and midwavelength infrared (MWIR) regions. The photocurrent, plotted as a function of light power for these four distinct bands, is fitted with the power law $I_{ph} \propto P^{\alpha}$ (Fig. 2f), where the extracted α values range from 0.96 to 1.03. The nearly linear dependence of I_{ph} on light power suggests the high quality of our device, as the presence of deep trap centers typically results in a sublinear relationship^{24,25} between I_{ph} and P. The vertical device exhibited negligible degradation after one month, revealing the effective protection effect of the graphene layers (Supplementary Fig. 10).

Comparative analysis of vertical and lateral channel device

To elucidate the superiority of vertical channels over lateral channels, we conducted a comparative analysis of their figure-of-merits performance metrics, including the external quantum efficiency (EQE), responsivity (R), specific detectivity (D^*), noise equivalent power (NEP) and response speed. All the measurements were performed at room temperature under zero bias voltage. The EQE is defined as the ratio of the number of collected charge carriers to the number of incident photons and can be calculated using the equation $EQE = Rhc/e\lambda$, where R represents the responsivity (defined as $R = I_{ph}/P$). In Fig. 3a, the wavelength-dependent EQE is presented for both the vertical Gr/BP/ MoS₂/Gr and lateral BP/MoS₂ photodetectors (Supplementary Fig. 11). The EQE of the vertical device is approximately one order of magnitude greater than that of the lateral channel device, exceeding 15% across a broad investigated wavelength range from 325 nm to 3600 nm. The higher charge carrier separation efficiency of the vertical heterostructure is also confirmed by the mid-infrared photoluminescence measurement (Supplementary Fig. 12). The responsivity of the vertical device once again demonstrates an order of magnitude improvement over that of the lateral channel device (Fig. 3b). In photovoltaic mode operation, where there is no photoconductive gain, the maximum achievable EQE is 100%. As a result, the maximum attainable R for a self-powered photodetector can be expressed $R = e\lambda/hc = \lambda/1240$ (the unit for wavelength here is nanometers). Notably, for our vertical device, a peak responsivity of 0.66 A/W is attained at a mid-infrared wavelength of 3600 nm (consistently surpassing 0.1 A/W across the investigated wavelength range), representing a remarkably high responsivity for a device operating in photovoltaic mode.

The specific detectivity D^* of a photodetector can be calculated using the formula $D^* = \sqrt{AB} \cdot R/I_n$. To extract D^* values, we measured the frequency-dependent noise spectral density for both the vertical and lateral channel devices. Various sources may contribute to the overall noise in photodetectors, including 1/f noise, shot noise, and thermal noise²⁶. As shown in Supplementary Fig. 13a, b, the noise power density spectra for both vertical and lateral devices exhibit a linear dependence on frequency in the low-frequency regime (f < 1 kHz), attributed to 1/f noise. Beyond 1 kHz, the noise power density remains nearly constant irrespective of the frequency, which is

indicative of white noise. At higher frequencies, two types of white noise, shot noise, and thermal noise, may contribute. The shot noise power density can be calculated by $\langle i_n^2 \rangle = 2eI_d$, where I_d is the dark current. In our device operating in photovoltaic mode with zero bias, the measured I_d is remarkably low, with a value of 6.36×10^{-12} A. Consequently, the $\langle i_n^2 \rangle$ induced by the shot noise is calculated to be 2.04×10^{-30} A²/Hz, two orders of magnitude lower than our measured noise level of 10⁻²⁸ A²/Hz. This indicates the negligible impact of shot noise in our device, with thermal noise dominating at high frequencies. From the measured noise power density spectra, we calculated the overall noise current across the bandwidth of 105Hz by $I_n = \sqrt{\int_1^B S_n(f) df}$. The calculated I_n values are $3.58 \times 10^{-12} \text{A}$ and 3.40×10^{-12} A for the vertical and lateral channel devices, respectively. This indicates that vertical devices operating at zero bias present a dark current similar to that of their lateral counterparts, coupled with the higher quantum efficiency of vertical devices, rendering them more suitable for high-performance photodetectors. As shown in Fig. 3c, the D^* of the vertical channel device consistently exceeds 3.88 × 10¹⁰ cmHz^{1/2}W⁻¹ across the wavelength range from 325 nm to 3800 nm and reaches a peak value of 2.38×10^{11} cmHz^{1/2}W⁻¹ at 3600 nm. The D* of the vertical device also demonstrated an order of magnitude improvement over that of the lateral channel device. Moreover, an ultralow noise equivalent power NEP of $1.72 \times 10^{-14} \, \text{WHz}^{-1/2}$ is achieved for the vertical device at 3600 nm (Supplementary Fig. 14).

Response speed is another crucial figure of merit for a photodetector. In general, the response time of a photodetector is limited by the RC time constant, carrier lifetime, and carrier transit time^{27,28}. By utilizing a highly resistive silicon substrate covered with silicon dioxide, the parasitic capacitance of the device can be effectively reduced. To further exclude the added capacitance induced by the chip carrier, high-frequency probes are designed for the vertical channel device (Supplementary Figs. 15, 16). Figure 3d shows the time-resolved photoresponse spectra measured with an oscilloscope under 1550 nm laser illumination modulated by an electro-optic modulator for the vertical device. The rise time (τ_r) and decay time (τ_d) for the vertical device are approximately 10.4 ns and 15.6 ns, respectively. We have fabricated three more vertical channel devices and measured their response speed using the high-frequency probes. All these devices exhibit response times below 20 ns, which are comparable to or even faster than the commercial mid-infrared HgCdTe photodetectors (Supplementary Fig. 17 and Supplementary Table 1). To reveal the response speed of the device in the mid-infrared region, we performed the pulsed laser measurements. As shown in Supplementary Fig. 18, the device's response speed is nearly identical in the visible, near-infrared, and mid-infrared ranges. Therefore, we can assume that the device's response speed measured at 1550 nm using an electro-optic modulator is representative of its response speed in the mid-infrared region. For the lateral device, τ_r and τ_d are approximately 3.6 μs and 3.9 μs , respectively, indicating a response time two orders of magnitude slower than that of the vertical device. Furthermore, the -3 dB cutoff frequency, a modulation frequency at which the photocurrent signal attenuates to 70.7% of its initial value, was determined from the frequency-dependent photoresponse. As shown in Fig. 3f, the -3 dB cutoff frequencies are 12 MHz and 40 kHz for the vertical and lateral devices, respectively. The response time τ can be extracted from the equation $R(f)/R_0 = 1/\sqrt{1 + (2\pi f \tau)^2}$, where R(f) and R_0 are the photoresponsivity under modulated and static light illumination, respectively²⁹. At the -3 dB cutoff frequency, $R(f)/R_0$ equals 0.707. Consequently, the corresponding response times τ are determined to be 13 ns and 3.98 us for the vertical and lateral devices, respectively, consistent with the response times extracted from time-resolved photoresponse spectra. For our vertical photodetector, both the carrier transit time and the RC time are estimated to be less than 1 ns

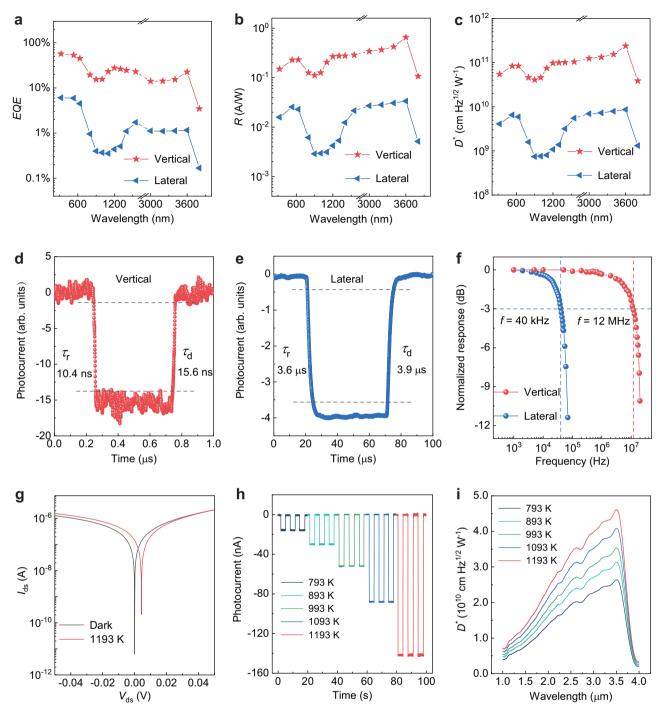


Fig. 3 | **Room-temperature performance comparison of photodetectors with vertical and lateral transport channels.** \mathbf{a} - \mathbf{c} Comparison of broadband wavelength-dependent external quantum efficiency (\mathbf{a}), responsivity (\mathbf{b}), and detectivity (\mathbf{c}) between vertical and lateral channel devices, with all measurements performed at $V_{\rm ds}$ = 0 V. \mathbf{d} , \mathbf{e} Rise and decay times for vertical (\mathbf{d}) and lateral channel devices (\mathbf{e}) measured at $V_{\rm ds}$ = 0 V under 1550 nm laser illumination. A digital oscilloscope was used to record the fast-varying photocurrent signals. \mathbf{f} Normalized

photoresponse as a function of modulation frequency extracted at $V_{\rm ds}$ = 0 V under 1550 nm laser illumination for vertical and lateral channel devices. **g** Output characteristics of the vertical photodetector in the dark and under illumination with 1193 K blackbody radiation. **h** Time-resolved photoresponse at different blackbody temperatures measured at $V_{\rm ds}$ = 0 V. **i** Wavelength-dependent D* of the vertical device at different blackbody temperatures measured at $V_{\rm ds}$ = 0 V.

(Supplementary Notes 2, 3 and Supplementary Figs. 19, 20). Therefore, the response time of a vertical photodetector is governed primarily by the material-specific carrier de-trap time. We anticipate that further improvements in response time could be achieved through the optimization of BP crystal growth conditions and device fabrication procedures. In contrast, the operational speed of the lateral device is

limited by the carrier transit time, which is estimated to be in the microsecond range (Supplementary Notes 2, 3 and Supplementary Fig. 21). It is important to note that the highly resistive silicon substrate plays a critical role in achieving the ultrafast response speed. For vertical devices fabricated on low-resistance silicon, the response speed is on the order of microseconds (Supplementary Fig. 22).

In practical applications of infrared photodetectors, a key figure of merit is their blackbody detection capability. Compared to that from lasers, the radiation from a blackbody source more accurately represents the actual radiation of the detected object. However, the characterization of most photodetectors based on 2D materials relies on lasers as the light source. Only a limited number of studies have explored the blackbody detection ability of these photodetectors^{11,12}. Figure 3g shows the *I–V* curves of the vertical device measured in the dark and under illumination by an 1193 K blackbody source. Notably, at zero bias voltage, a significant increase in the current is observed upon exposure to blackbody radiation, indicating the excellent blackbody responsivity of our vertical photodetector. Figure 3h shows the timeresolved photoresponse spectra measured at different blackbody temperatures. The photocurrent gradually increases with increasing blackbody temperature. This can be attributed to the combined effects of temperature-dependent spectral radiance and wavelengthdependent photoresponse. The overall photocurrent at different blackbody temperatures should be proportional to $\int_0^\infty S(\lambda) \cdot M(\lambda, T) d\lambda$, where $S(\lambda)$ is the relative spectral response of the photodetector, and $M(\lambda,T)$ is the spectral radiant exitance of a blackbody following Plank's Law $M(\lambda, T) = 2\pi hc^2/(\lambda^5 \cdot (\exp(\frac{hc}{\lambda kT}) - 1))$ (Supplementary Fig. 23). To elucidate the underlying physics of the temperature-dependent photo response, we measured the $S(\lambda)$ of the vertical photodetector using a Fourier transform infrared spectrometer (Supplementary Fig. 24) and calculated $\int_0^\infty S(\lambda) \cdot M(\lambda, T) d\lambda$ at different temperatures. The integrated value indeed increases with increasing temperature (Supplementary Fig. 25), which is consistent with our experimental observations. The blackbody detectivity D_h^* is calculated according to $D_h^* = \sqrt{AB} \cdot I_{nh}/(I_n \cdot P)$, where P represents the blackbody radiation power incident on the device; the calculation details are presented in the methods section. The temperature dependence D_h^* of the vertical device is shown in Supplementary Fig. 26. Notably, D_b^* gradually increases with increasing temperature (Supplementary Note 4), and a D_b^* value of 2.96×10^{10} cmHz^{1/2}W⁻¹ is obtained at 1193 K radiation. The peak blackbody detectivity D_p^* can be extracted using the following formula12:

$$D_{p}^{*} = D_{b}^{*} \cdot \int_{0}^{\infty} M(T, \lambda) d\lambda / \int_{0}^{\infty} S(\lambda) \cdot M(T, \lambda) d\lambda$$
 (2)

The wavelength-dependent D^{*} values at different blackbody temperatures are extracted and plotted in Fig. 3i, where a D_{p}^{*} of 4.61×10^{10} cmHz^{1/2}W⁻¹ is achieved at 3500 nm at 1193 K. The relatively lower detectivity of the blackbody measurement compared with the laser measurement can be attributed to the anisotropy of black phosphorus (Supplementary Fig. 27). We also characterized the blackbody detection capability of the lateral channel device, which has a D^{*} value one order of magnitude lower than that of the vertical device across the measured wavelength (Supplementary Fig. 28).

Impact of channel length scaling on device performance

To directly elucidate the influence of the channel length on the photoelectric conversion process of the device, we fabricated six pairs of electrodes on a single BP/MoS $_2$ heterojunction. In each electrode pair, one is deposited on BP, and the other is deposited on MoS $_2$, effectively creating six devices with different lateral channel lengths. As shown in Fig. 4a, BP and MoS $_2$ are highlighted by yellow and blue lines, respectively. The overlapping region in the middle represents the heterojunction area. Moreover, AFM measurements revealed that the thicknesses of the BP and MoS $_2$ layers were 34 nm and 24 nm, respectively (Supplementary Fig. 29). This device exhibits a low noise power density under zero bias (Supplementary Fig. 30). We compared the output curves of all sets of devices with different channel lengths varying from 13.7 μ m to 112.3 μ m. Clear rectifying characteristics are observed for all the devices, indicating the formation of an effective

p-n junction. Under forward bias, I_{ds} gradually decrease with increasing channel length, which is attributed to the increased channel resistance (Supplementary Fig. 31). For the photoresponse measurements, all the devices were operated in zero-bias photovoltaic mode. The incident light is focused onto the overlapped heterojunction without irradiating the surrounding regions. This measurement setup ensures that, for the six different devices, the generation and separation processes of photogenerated charge carriers remain consistent, with the only distinction lying in the carrier diffusion processes within channels of different lengths. Figure 4b shows the time-resolved photoresponse under 1550 nm focused laser illumination. The photocurrent gradually decreases with increasing channel length. Consequently, the extracted R and EQE also decrease fourfold as the channel length increases from 13.7 µm to 112.3 µm (Fig. 4c). This result clearly reveals the issue of diffusion loss of photogenerated charge carriers for long-channel devices, where electrons and holes recombine before reaching the electrodes. The response time is also extracted for six devices with varying channel lengths. Notably, both the rise time and decay time increase with channel length, showing a variation of more than one order of magnitude: from 1.74 µs and 1.92 µs for a 13.7 µm channel to 19.86 µs and 42.2 µs for a 112.3 µm channel (Fig. 4d and Supplementary Fig. 32). By further decreasing the channel length of the lateral channel device to ~1 µm, the response speed can be improved to as fast as 436 ns (Supplementary Fig. 33).

Benchmarking against other room temperature MWIR photodetectors

Figure 5a shows a comparison of the wavelength-dependent D^* of the Gr/BP/MoS₂/Gr vertical channel photodetector with those of other room-temperature-operated MWIR photodetectors utilizing both 2D materials with lateral transport channels^{11–13,15,16} and conventional bulk materials. It is clear that the vertical device demonstrates superior performance in terms of both high detectivity and ultrabroadband detection range. The D^* of the vertical device measured over the entire investigated wavelength range (325 nm to 3800 nm) exceeded $3.88 \times 10^{10} \text{ cmHz}^{1/2}\text{W}^{-1}$. Notably, at 3600 nm, a detectivity of 2.38 × 10¹¹ cmHz^{1/2}W⁻¹ is achieved, approaching the theoretical limit constrained by BLIP. Fast and sensitive photodetection is a critical benchmark for high-performance photodetectors. Figure 5b compares the performance of the vertical device with that of other reported 2D material photodetectors with MWIR responses in terms of both detectivity and response speed^{11-13,15,16,30-35}. Our device response speed and detectivity are among the highest of those reported for comparable 2D material devices, reaching or even surpassing the response speed of commercial cooled HgCdTe photodetectors. Comprehensive comparisons of the mid-infrared performance of our device with commercial HgCdTe photodetectors and various narrow-gap 2D materials are provided in Supplementary Tables 1 and 2, respectively. It is worth mentioning that the response speed of our device is directly extracted from a complete periodic cycle by modulating the light onoff with an electro-optic and acousto-optic modulator, which allows the photocurrent to rise and fall to a stable value in each cycle. Several reported works use a pulsed laser to characterize the response speed, where the maximum photocurrent is limited by the pulse width of the laser and does not rise to a stable value, leading to an overestimation of the response speed. The response speed of our device surpassed that of other devices in the microsecond range, reaching the nanosecond range, leading to significant advancements in 2D material-based MWIR photodetectors.

Discussion

In summary, we have simultaneously achieved high-sensitivity, highspeed, and ultrabroadband mid-infrared detection within a single photodetector by implementing a 2D heterostructure with a vertical transport channel. The impact of channel length scaling on both the

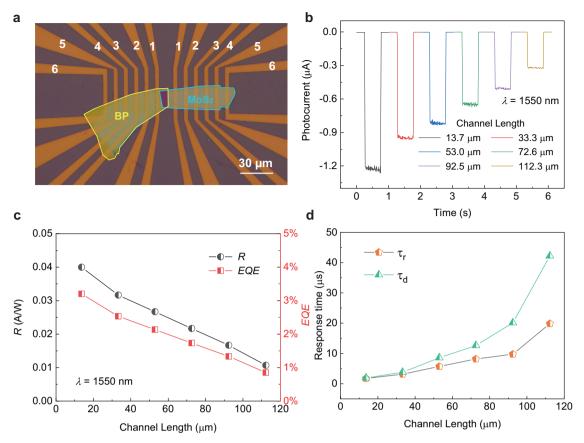


Fig. 4 | Effect of channel length scaling on the photoresponse properties of lateral channel devices. a Optical image of a BP/MoS $_2$ heterojunction with six pairs of electrodes of different channel lengths varying from 13.7 μm to 112.3 μm . b Timeresolved photoresponse for lateral devices with different channel lengths

measured at $V_{\rm ds}$ = 0 V under 1550 nm laser illumination. **c** Responsivity and external quantum efficiency as a function of lateral channel length under 1550 nm laser illumination at $V_{\rm ds}$ = 0 V. **d** Extracted rising time and decay time as a function of lateral channel length under 633 nm laser illumination at $V_{\rm ds}$ = 0 V.

external quantum efficiency and response speed is clearly elucidated, demonstrating the superiority of vertical 2D photodetectors over commonly used lateral counterparts. Our Gr/BP/MoS₂/Gr vertical photodetector is a new benchmark with a high MWIR of 2.38 × 10¹¹ cmHz^{1/2}W⁻¹ approaching the theoretical limit, a fast response speed of 10.4 ns at 1550 nm, and an ultrabroadband detection range spanning from the ultraviolet to mid-infrared region. The overall room-temperature performance of our vertical device is comparable or even superior to the commercial cooled mid-infrared HgCdTe photodetectors. We anticipate that our findings will significantly propel the advancement of next-generation high-performance infrared photodetectors operating at room temperature.

Methods

Device fabrication

For the fabrication of the vertical channel device, the bottom electrode (5 nm Ti and 30 nm Au) was prepared through laser lithography patterning and subsequent thermal evaporation on a high-resistance (4000 Ω -cm) silicon substrate coated with 300 nm SiO_2 . A top finger electrode (30 nm Au) was initially fabricated on an intrinsic silicon substrate. The finger electrode was then coated with PMMA resist by spin coating and subsequently lifted off from the substrate using polydimethylsiloxane (PDMS), which served as a transfer electrode for later use. The bottom graphene, MoS $_2$ flakes, BP flakes and top graphene were mechanically exfoliated from bulk crystals and sequentially stacked layer by layer on the prepared bottom electrode by a dry transfer method. All 2D materials used in this work were purchased from HQ Graphene. To prevent BP from undergoing ambient

oxidation, both the exfoliation and transfer processes were conducted in an argon-purged glovebox with oxygen and moisture concentrations lower than 0.1 ppm. Finally, the prepared top electrode was transferred onto the heterostructures to complete the fabrication of the vertical device. For the fabrication of lateral channel devices, both the source and drain electrodes (30 nm Au) were initially fabricated on an intrinsic silicon substrate and then lifted off as the transfer electrodes for the BP/MoS $_2$ heterojunction.

Device characterization

The thicknesses of the MoS₂ and BP flakes were determined using atomic force microscopy (AFM, Bruker Dimension Icon). Raman spectroscopy and photocurrent mapping were conducted on a WITec Alpha300R system equipped with a 633 nm diode-pumped solid-state laser. Electrical and optoelectrical characterizations of the devices were carried out using a semiconductor parameter analyzer (FS-Pro, PRIMARIUS) at room temperature under ambient conditions. Various light sources, ranging from ultraviolet to mid-infrared, were employed to assess device performance. These sources include monochromatic lasers at wavelengths of 325, 532, and 633 nm, a Ti:sapphire femtosecond laser (680-1600 nm, 80 MHz, Chameleon Compact OPO), and a tunable mid-infrared laser (2.8-4 µm, Cati-T-3-4, BEST RAY). For the high-frequency probe measurement, a 1550 nm laser was modulated by an electro-optic modulator (MXAN-LN-40). For the chip carrier measurement, a 633 nm laser was modulated by an acousto-optic modulator (R21080-1DS). A digital oscilloscope (MDO3032, Tektronix) was used to record the transient photocurrent signal. The relative response spectrum was measured by a Fourier transform infrared

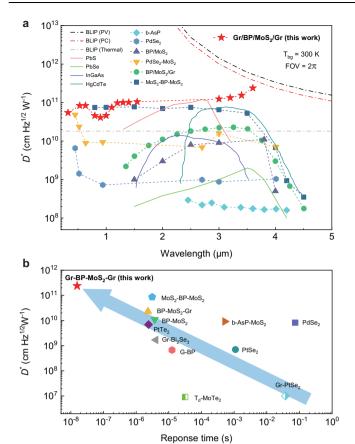


Fig. 5 | Comparison of the room temperature performances of the vertical channel photodetector and other reported photodetectors. a Comparison of the detectivity and detection range among reported room temperature-operated mid-wave infrared (MWIR) photodetectors based on 2D materials and conventional materials $^{11-13,15,16}$. The theoretical limits of D^* calculated for the photodetectors operating under background-limited infrared performance (BLIP) in photovoltaic (PV) mode, photoconductive (PC) mode, and thermal infrared (TIR) mode are shown as black, red, and blue dotted lines, respectively. T_{bg} and FOV represent background temperature and field of review. **b** Comparison of the detectivity and response speed among reported room temperature-operated photodetectors based on 2D materials with MWIR (3–6 μm) responses $^{11-13,15,16,30-35}$.

spectrometer (Nicolet 8700) at room temperature. For the pulsed laser measurement, the pulses with 800 nm central wavelength and 35-fs pulse width at 1 kHz repetition rate was provided by Ti:sapphire regenerative amplifier laser system (Astrella, Coherent). Optical parametric amplifier (OPA) extended the wavelength to 633, 1550, and 3000 nm (OPerA Solo, Coherent). A chopped laser with a 429 Hz chopper frequency, 532 nm wavelength, ~25 μm spot radius, and laser power density of 90 Wcm $^{-2}$ was used as an excitation source for the PL measurement. The PL signal was collected via 15 × objective and further analyzed by FTIR spectrometer.

Blackbody measurements

Blackbody response measurements were performed at room temperature under ambient conditions with a calibrated commercial blackbody source (HFY-200C). The power incident on the effective area of the device can be calculated by $P = \alpha \varepsilon \sigma (T_b^4 - T_0^4) A_d R^2 / L^2$, where α is the modulation factor (1.0), ε is the average emissivity of the blackbody radiation source (0.9), σ is the Stefan–Boltzmann constant, T_b is the blackbody source temperature (793 K – 1193 K), T_0 is the room temperature (300 K), A_d is the effective device area, R is the selected aperture radius of the blackbody radiation source (0.5 cm), and L is the distance between the aperture and the device surface (5 cm). It is

noteworthy that the modulation factor in our measurement setup is 1.0, rather than the usually reported 0.35 for lock-in measurements. This is because our time-resolved blackbody response was directly measured by the semiconductor parameter analyzer without high-frequency light modulation. However, the blackbody response measured by a lock-in amplifier usually requires the incident light to be modulated, which results in a photocurrent amplitude modulation of 0.35 of its maximum value.

Data availability

Relevant data supporting the key findings of this study are available within the article and the Supplementary Information file. All raw data generated during the current study are available from the corresponding authors upon request.

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Author contributions

Z.N., J.L., and J.Z. conceived the idea and designed the experiments. J.W. fabricated all the devices. J.W. and J.Z. carried out the optoelectronic measurements with the help of W.W., Z.H., and Y.Y. J.W., H.L., D.W., H.W., T.Z., and Y.C. performed the response time measurement. J.W., W.W., Q.F., and R.L. performed the Raman measurements. J.W. and X.Z. conducted the AFM measurements. R.J. and W.H. performed the FTIR measurements. H.L., X.C., and S.C. performed the PL measurements. J.W., J.Z., J.L., and Z.N. co-wrote the manuscript. All the authors discussed the results and reviewed the manuscript.

Competing interests

The authors declare no competing interests.

Additional information

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