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# Terahertz spin torque nano-oscillator based on a ferrimagnetic skyrmion lattice

Laichuan Shen<sup>1</sup>, Qiming Shao<sup>2,3</sup>, Johan Åkerman<sup>4,5,6</sup> & Yan Zhou<sup>1</sup> ✉

Spin torque nano-oscillators have received continuously increasing attention due to their rich dynamics and potential applications. Here, we propose a spin torque nano-oscillator based on a ferrimagnetic skyrmion lattice, where the weak Magnus forces together with intriguing skyrmion-skyrmion interactions allow current-driven skyrmions to oscillate at terahertz frequencies. Through micromagnetic simulations, we demonstrate that a small current injection area results in identical motion orbits for the oscillating skyrmions, while a large injection area yields distinct or even chaotic trajectories. We analyze the transition between identical and distinct orbits using the Thiele equation, which also explains the parameter dependence of the oscillator frequency. In addition, synchronized oscillation signals emitted from a single oscillator are demonstrated. Our results not only reveal the high-frequency oscillation dynamics of ferrimagnetic skyrmions, but also pave the way for developing skyrmion-based oscillators.

Spin torque nano-oscillators, capable of generating persistent oscillatory signals through current-induced spin torque fully compensating the system dissipation, have attracted considerable attention due to their intriguing dynamics and important applications in microwave communication and neuromorphic computing<sup>1–11</sup>. To date, various nano-oscillators based on magnetic textures, including uniform magnetizations<sup>1,12–15</sup>, vortices<sup>4,7,16–18</sup>, droplets<sup>19–24</sup>, bimerons<sup>25</sup> and skyrmions<sup>26–36</sup>, have been proposed. Among these, skyrmion-based nano-oscillators are expected to deliver enhanced output power and reduced linewidth<sup>26</sup>. However, reported designs typically allow skyrmion oscillations only at moderate frequencies—often below 40 gigahertz (GHz)<sup>26–28,30,31</sup>.

In ferromagnetic skyrmion oscillators, this frequency limitation stems mainly from the difficult-to-balance Magnus force acting on the moving skyrmion. In contrast, antiferromagnetic skyrmion oscillators require an additional strong force to act as the velocity-dependent centripetal force<sup>28</sup>. Recent theoretical studies have demonstrated that the Magnus force in ferrimagnetic skyrmions is highly tunable<sup>37,38</sup>, making it a promising mechanism for providing a suitable centripetal force. This finding opens up new possibilities for achieving high-frequency skyrmion oscillations.

In general, the implementation of most proposed skyrmion oscillators requires the generation of a single skyrmion or a given number of skyrmions at a specified location in the nanoscale magnetic layer<sup>26–28,30,31,37–39</sup>, which increases fabrication complexity and cost. However, skyrmions in magnetic materials often naturally form lattices, such as triangular lattices<sup>40–43</sup>. These

skyrmion lattices inherently exhibit skyrmion-skyrmion interactions, making them ideal for supporting rotational motion along well-defined orbits. While temperature-gradient driven rotation of skyrmion lattices has been reported<sup>44</sup>, the dynamics under localized driving current injection remain unexplored, which greatly motivates the present work.

In this study, we use micromagnetic simulations to investigate the dynamics of ferrimagnetic skyrmion oscillators with a skyrmion lattice as the initial state. We find that such ferrimagnetic skyrmions can oscillate at terahertz (THz) frequencies, exhibiting identical, distinct, or even chaotic motion trajectories, depending on the current injection areas. Theoretical analysis based on the Thiele equation explains the parameter dependence of oscillator frequency and the transition of the skyrmion trajectories. We also show that multiple skyrmions within a single oscillator can produce synchronized oscillation signals, offering a pathway toward high-power THz signal generation.

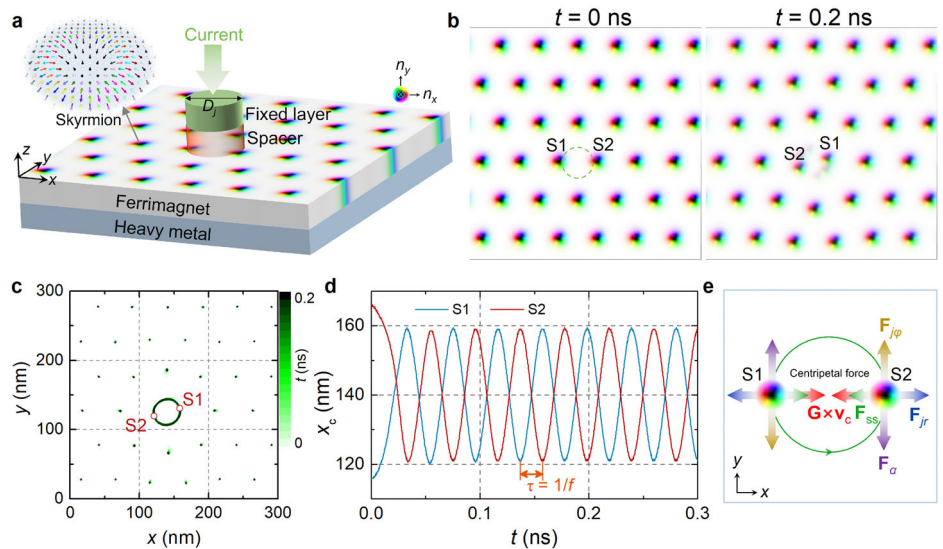
## Results and discussion

### Theoretical model

The geometry of our ferrimagnetic skyrmion oscillator is depicted in Fig. 1a, where the magnetic working layer is a ferrimagnet with a regular skyrmion lattice, stabilized by the interfacial Dzyaloshinskii-Moriya interaction (DMI)<sup>45,46</sup> induced by the heavy metal. A circular current injector with diameter  $D_j$ , placed on top of the ferrimagnet, drives the skyrmion dynamics through current-induced spin transfer torques<sup>47,48</sup>, which can also be used to

<sup>1</sup>School of Science and Engineering, The Chinese University of Hong Kong, Shenzhen, Guangdong, China. <sup>2</sup>Department of Electronic and Computer Engineering, The Hong Kong University of Science and Technology, Kowloon, Hong Kong SAR. <sup>3</sup>Department of Physics, The Hong Kong University of Science and Technology, Kowloon, Hong Kong SAR. <sup>4</sup>Department of Physics, University of Gothenburg, Gothenburg, Sweden. <sup>5</sup>Center for Science and Innovation in Spintronics, Tohoku University, Sendai, Japan. <sup>6</sup>Research Institute of Electrical Communication, Tohoku University, Sendai, Japan. ✉e-mail: [zhouyan@cuhk.edu.cn](mailto:zhouyan@cuhk.edu.cn)

**Fig. 1 | Spin torque oscillator based on a ferromagnetic skyrmion lattice.** **a** Schematic of the proposed nano-oscillator comprising a ferrimagnet with a regular skyrmion lattice. The heavy metal underneath the ferrimagnet induces Dzyaloshinskii-Moriya interaction to stabilize the skyrmions, while the circular current injector with diameter  $D_j$  is used to excite the skyrmion dynamics. **b** Snapshots of the skyrmion configurations at two different simulation times. The skyrmions driven directly by the current are labeled as S1-S2, with the edge of the current injector indicated by the green dashed circle. The black (white) areas denote the Néel vector along  $-z$  ( $+z$ ), and the colors indicate the in-plane orientation. **c** Skyrmion trajectories and **d** the  $x$ -component of the location ( $x_c$ ) of skyrmions S1 and S2. Skyrmion trajectories are obtained by recording the evolution of the coordinates of the grid points with  $n_z \sim -1$ . **e** Force analysis of the skyrmions.  $F_{j\varphi}$  and  $F_{jr}$  are the azimuthal and radial current-induced forces, respectively.  $F_\alpha$ ,  $F_{ss}$ , and  $\mathbf{G} \times \mathbf{v}_c$  denote the frictional force, the skyrmion-skyrmion interaction force, and the Magnus force, respectively.



electrically read out the skyrmion oscillations and may influence the properties of the working layer, with limited effects expected<sup>49</sup>. We use the micromagnetic simulation package MUMAX3<sup>50</sup> to study the current-induced dynamics. The simulation details and relevant material parameters are provided in the Methods and Supplementary Note 1. The obtained snapshots of the Néel vector  $\mathbf{n} = (\mathbf{m}_1 - \mathbf{m}_2)/2$  (with the reduced magnetizations  $\mathbf{m}_{1(2)}$ ) and skyrmion trajectories are shown in Fig. 1b,c, respectively. As seen, the skyrmions (labeled S1 and S2) driven directly by the current perform a nearly circular motion, where the boundary of the current injection area is illustrated by a dashed circle in Fig. 1b. From the time evolution of the skyrmion location shown in Fig. 1d, we find that the oscillator's output frequency  $f$  reaches a relatively high value of  $\sim 49$  GHz.

To understand the mechanisms behind the high-frequency skyrmion oscillation, we employ the Thiele equation<sup>38,51–54</sup> to analyze the forces acting on the skyrmions. According to previous works<sup>37,55</sup>, the Thiele equation of the  $i$ th ferrimagnetic skyrmion reads:

$$m_{\text{eff},i} \ddot{\mathbf{r}}_{c,i} = \mathbf{G} \times \dot{\mathbf{r}}_{c,i} + \mathbf{F}_{\alpha,i} + \mathbf{F}_{j,i} + \mathbf{F}_{ss,i}, \quad (1)$$

where  $m_{\text{eff}}$  is the effective mass and  $\mathbf{r}_c = (x_c, y_c)$  is the position coordinate of the skyrmion center, which can be defined by averaging the topological density  $\rho_t$  of the magnetic structure, i.e.,  $\mathbf{r}_c = \int \rho_t d\mathbf{x} d\mathbf{y} / \int \rho_t d\mathbf{x} d\mathbf{y}$  with  $\rho_t = 1/(4\pi) \mathbf{n} \cdot (\partial_x \mathbf{n} \times \partial_y \mathbf{n})$ <sup>56</sup>. The term  $\mathbf{G} \times \dot{\mathbf{r}}_c$  stands for the Magnus force with the gyrovector  $\mathbf{G}$ <sup>57,58</sup>.  $\mathbf{F}_\alpha = -\alpha L \dot{\mathbf{r}}_c$  is the frictional force with the damping constant  $\alpha$  and dissipation coefficient  $L$ .  $\mathbf{F}_j = -(j\hbar P/e) \mathbf{u}$  is the current-induced force with  $j$  being the current density,  $\hbar$  the reduced Planck constant,  $P$  the spin polarization efficiency and  $e$  the elementary charge<sup>55</sup>.  $u_i = \int_A (\mathbf{n} \times \mathbf{p}) \cdot \partial_i \mathbf{n} d\mathbf{x} d\mathbf{y}$  with  $i = x, y$  is related to the polarization vector ( $\mathbf{p}$ ) and the current injection area ( $A$ ). The last term of the Thiele equation  $\mathbf{F}_{ss}$  is the repulsive force between skyrmions<sup>37,59,60</sup>. These forces are schematically depicted in Fig. 1e with the subscript  $\varphi$  ( $r$ ) indicating the azimuthal (radial) component of forces, while more details of them are provided in the Methods.

The radial force balance suggests that the realization of high-frequency oscillation requires a relatively weak Magnus force  $\mathbf{G} \times \dot{\mathbf{r}}_c$  acting on the high-speed skyrmion, as the other radial forces,  $\mathbf{F}_{ss}$  and  $\mathbf{F}_{jr}$ , are not directly related to the skyrmion velocity. The reduction of Magnus force here is achieved using the unique properties of ferrimagnet. Specifically, the opposite and different magnetic moments on the two sublattices of the ferrimagnet give rise to a small value of  $G \propto (M_{s1}/\gamma_1 - M_{s2}/\gamma_2)$  with the saturation magnetization  $M_{s1(2)}$  and gyromagnetic ratio  $\gamma_{1(2)}$ <sup>38,58</sup>.

From the azimuthal force balance, i.e.,  $\mathbf{F}_\alpha + \mathbf{F}_{j\varphi} \approx \mathbf{0}$ , we derive the frequency ( $f$ ) of the skyrmion oscillators

$$f = N_{\text{sky}} \frac{F_{j\varphi}}{2\pi R_c \alpha L}, \quad (2)$$

where  $N_{\text{sky}} = 2$  is the number of rotating skyrmions<sup>26</sup> and  $R_c$  is the orbit radius.

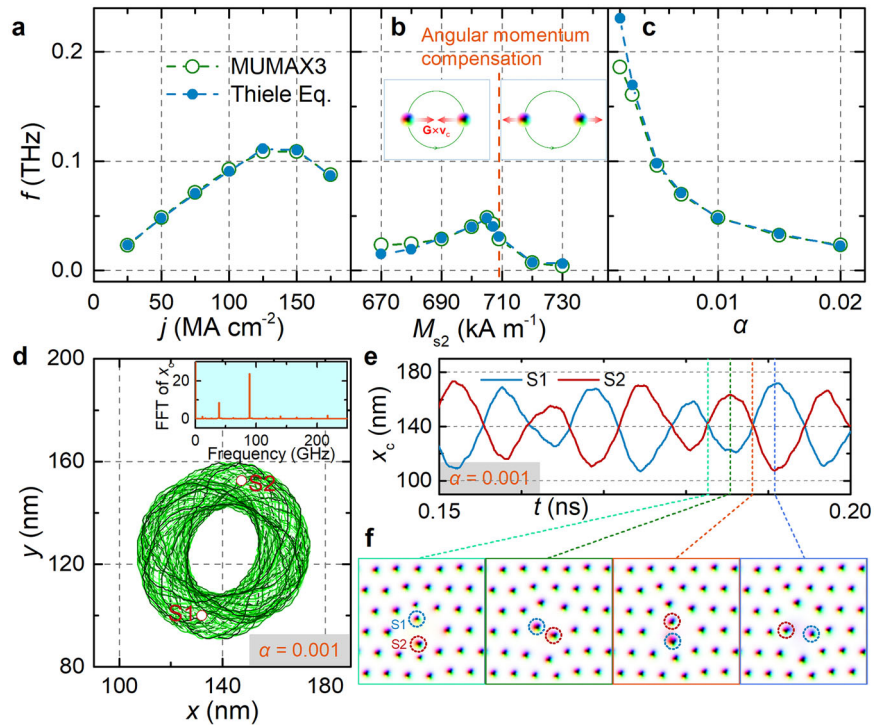
### Parameter dependence of skyrmion dynamics

Figure 2a–c compare the frequencies obtained from simulations and Eq. (2) with different values of the current density  $j$ , saturation magnetization  $M_{s2}$ , and damping constant  $\alpha$ . The results of Eq. (2) with numerical  $F_{j\varphi}$  and  $R_c$  (see Supplementary Fig. 2) agree well with those from the simulations. As shown in Fig. 2a, the frequency exhibits a non-monotonic behavior with increasing current. This is due to the non-monotonic variation of the driving force  $F_{j\varphi}$  induced by the change in orbit radius  $R_c$  (Supplementary Fig. 2). Note that small currents ( $j < 15 \text{ MA cm}^{-2}$ ) cannot sustain persistent skyrmion oscillation, while large currents ( $> 250 \text{ MA cm}^{-2}$ ) lead to the annihilation of the skyrmions. As the saturation magnetization  $M_{s2}$  is increased from 670 to 730  $\text{kA m}^{-1}$ , we also observe a non-monotonic change in the frequency [see Fig. 2b]. This can be understood from the fact that when increasing  $M_{s2}$  (with fixed  $M_{s1} = 709 \text{ kA m}^{-1}$ ), the Magnus force weakens and even reverses at the angular momentum compensation point ( $G = 0$ ), which results in the skyrmions S1 and S2 moving away from each other hence tracing out a larger orbit. As shown in Fig. 3d and Supplementary Fig. 2, the increased orbit radius yields a non-monotonic driving force, explaining the non-monotonic relation between  $M_{s2}$  and  $f$ . In Fig. 2c, one may notice that the oscillation frequency increases as the damping decreases, which is attributed to the improvement in driving efficiency at low magnetic damping, as expected from Eq. (2). More importantly, the calculation results demonstrate that the frequency of our proposed oscillator can reach about 0.2 THz, which is much higher than that of other skyrmion-based oscillators (see Supplementary Note 3 for the details of frequency comparisons)<sup>28,30,31,37</sup>. When the damping is reduced to 0.001, the skyrmion trajectory becomes irregular [see Fig. 2d] and the orbit radius changes over time [Fig. 2e], corresponding to multi-frequency oscillations, as observed in the frequency spectrum in the inset of Fig. 2d. The formation of such a trajectory originates from the change in skyrmion size during their rotation, as shown in Fig. 2f; details of the skyrmion dynamics are provided in Supplementary Movie 1. Additionally, the influences of the defects, Oersted

**Fig. 2 | Frequency of the skyrmion oscillator.**

Dependence of the skyrmion oscillation frequency on **a** the current density  $j$ , **b** saturation magnetization  $M_{s2}$  and **c** damping constant  $\alpha$ . Solid circles represent analytical results from the Thiele equation; open circles indicate simulation results. Default parameters:  $j = 50 \text{ MA cm}^{-2}$ ,  $D_j = 40 \text{ nm}$ ,  $M_{s1} = 709 \text{ kA m}^{-1}$ ,  $M_{s2} = 705 \text{ kA m}^{-1}$  and  $\alpha = 0.01$ .

**d** Trajectories and **e**  $x$ -component of the location ( $x_c$ ) of skyrmions S1 and S2 with  $\alpha = 0.001$ . The inset in **d** shows the Fast Fourier transform (FFT) of  $x_c(t)$ . **f** A sequence of snapshots of the skyrmions.



fields and local anisotropy variations on skyrmion dynamics are discussed in the Supplementary Information.

We next examine how the current injector diameter  $D_j$  affects the skyrmion dynamics. Figure 3a–c depict the time evolution of the skyrmion trajectories for injector diameters  $D_j = 45, 46$  and  $70 \text{ nm}$ , respectively. Here, we take the magnetic structure shown in Fig. 1b as the initial state, with the horizontal distance between the centers of adjacent skyrmions being  $50 \text{ nm}$ . With  $D_j = 45 \text{ nm}$ , skyrmions S1 and S2 move in orbits with the same radius. However, for a slightly larger injector with  $D_j = 46 \text{ nm}$ , their orbits have different radii. To analyze the transition between the two distinct trajectories presented in Fig. 3a,b, we derive the equation for the orbit radii of the skyrmion S1 and S2 (see Supplementary Note 2 for derivation details), described as

$$b \equiv \frac{m_{\text{eff}} F_{j\varphi}^2}{G\alpha L F_{j\varphi} - \alpha^2 L^2 (F_{jr} + F_{ssr})} = R_c, \quad (3)$$

where  $F_{ssr}$  is the radial component of the skyrmion-skyrmion interaction force. For simplicity, we treat  $(F_{jr} + F_{ssr})$  in Eq. (3) as a constant, since  $F_{j\varphi}$  is the dominant term over  $F_{jr}$  and  $F_{ssr}$ . Thus, the solution of Eq. (3) requires the acquisition of parameter  $b$ , more specifically, specifying the expression of  $F_{j\varphi}$  with respect to  $R_c$  and  $D_j$ . In order to obtain  $F_{j\varphi}(R_c)$ , we perform micromagnetic simulations with a ferrimagnetic skyrmion undergoing centrifugal motion driven by the current, following our previous work<sup>55</sup>. Such a centrifugal motion is achieved by setting a relatively large value of  $M_{s2} = 720 \text{ kA m}^{-1}$ . Based on the magnetic structures of skyrmion during centrifugal motion, we compute the driving forces  $F_{j\varphi}$  with different values of  $D_j$  and fit them using the formula  $F_{j\varphi} = k_1 \exp\{-[(R_c - D_j/2)/k_2]^{k_3}\}$  with  $k_1 = 32.78 \times 10^{-13} \text{ N}$ ,  $k_2 = 37 \text{ nm}^2$  and  $k_3 = 0.728$ , as shown in Fig. 3d. It can be seen that the  $F_{j\varphi}(R_c)$  curves exhibit a simple horizontal shift as  $D_j$  changes. With the above expression of  $F_{j\varphi}$  and the value of  $(F_{jr} + F_{ssr}) \sim 1.48 \times 10^{-13} \text{ N}$  at  $D_j = 45 \text{ nm}$ , we plot the parameter  $b$  in Fig. 3e with different values of  $D_j$ . As seen, once  $D_j$  is greater than  $\sim 46 \text{ nm}$ , the parameter  $b$  no longer intersects with  $R_c$ , resulting in the breakdown of Eq. (3) and therefore the occurrence of a transition in the skyrmion trajectories. As shown in the Supplementary Fig. 5, identical and distinct skyrmion trajectories can be

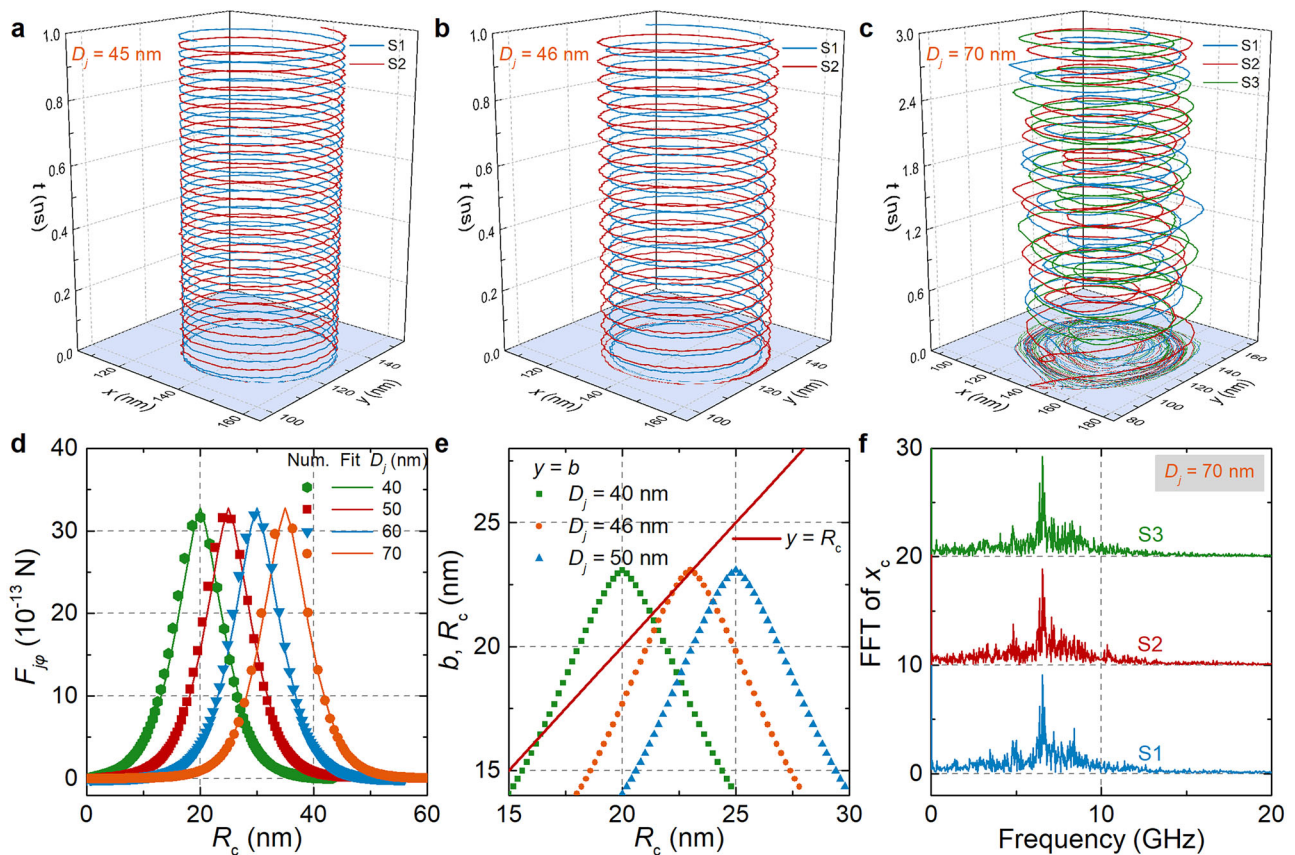
found at certain locations of the injector center. Note that for the case  $D_j = 40 \text{ nm}$  in Fig. 3e, there are two intersection points: one corresponds to a stable orbit and the other to an unstable fixed point<sup>38</sup>.

More interestingly, at  $D_j = 70 \text{ nm}$ , the number of skyrmions directly driven by current increases from two to three (S1–S3), and the skyrmion trajectories show no regularity at all [see Fig. 3c], suggesting the emergence of chaos. To confirm the chaotic trajectories, we perform a Fast Fourier transform of the skyrmion position [Fig. 3f], revealing a broadband, noise-like frequency spectrum characteristic of chaos<sup>55,61</sup>. For a more precise validation of chaotic trajectories, we calculate the Lyapunov exponent of  $x_c(t)$  of skyrmion S1 using the method proposed by Rosenstein et al.<sup>62</sup>, and indeed find a positive Lyapunov exponent of  $\sim 2.1 \text{ ns}^{-1}$  as a signature of chaos. Additional details of the skyrmion dynamics in the above three cases with  $D_j = 45, 46$  and  $70 \text{ nm}$  are provided in Supplementary Movie 2–4, respectively.

### Extension to many-skyrmion oscillations

In this section, we further expand the current injection area in micromagnetic simulations to demonstrate many-skyrmion oscillations and provide a promising method to improve the power output of skyrmion oscillators. A rectangular strip-shaped injector ( $460 \times 40 \text{ nm}^2$ ) [see Fig. 4a], smaller than the ferrimagnet's top surface ( $500 \times 200 \text{ nm}^2$ ), is used to induce multiple well-defined skyrmion trajectories. When the current is applied to the injector, the skyrmions in the middle region of the ferrimagnet rotate counterclockwise around the injection area, as indicated by the green arrows in Fig. 4b. While the detailed dynamics of skyrmions can be seen in Supplementary Movie 5, we plot the skyrmion trajectories in Fig. 4c. The ferrimagnetic skyrmion oscillations can be detected using similar magnetoresistance measurements that have been utilized for ferromagnets<sup>49,63,64</sup>, thanks to the property of ferrimagnets with two inequivalent sublattices<sup>65</sup>. The magnetoresistance actually reflects the magnetizations of output regions. Specifically, if the detector and the ferrimagnetic working layer form a magnetic tunnel junction (MTJ), the MTJ resistance can be described as  $R_{\text{MTJ}} = R_p + (R_{\text{AP}} - R_p)(1 - n_z)/2$  for the magnetizations of the fixed layer of the detector along the  $z$  direction, with  $R_p$  ( $R_{\text{AP}}$ ) being the resistance of parallel (antiparallel) state of the MTJ<sup>66</sup>. Here we take seven equally spaced regions as output areas [black squares in





**Fig. 3 | Skyrmion trajectories for different current injector diameters.** **a** Injector diameters  $D_j = 45$  nm, **b** 46 nm and **c** 70 nm. **d** Azimuthal current-induced forces  $F_{\phi}$  as a function of orbit radius  $R_c$  for different injector diameters  $D_j$ . Symbols represent

numerical results; solid curves are fitted expressions. **e** Dependence of parameter  $b$  on  $R_c$  with different values of  $D_j$ . **f** Fast Fourier transform of  $x_c(t)$  for  $D_j = 70$  nm, showing a broad spectrum characteristic of chaos.

Fig. 4b, O1–O7] and present the recorded out-of-plane Néel vector  $n_z$  of these areas in Fig. 4d with different spacings  $d$  of output areas. The sum of  $n_z$  of all output regions is plotted in Fig. 4e with  $A_s$  representing the oscillation amplitude. It can be seen that the total amplitude ( $A_s$ ) is much larger than that of a single output area ( $\sim 0.5$ ), thus yielding an improved power output  $P_{\text{out}} \propto |A_s|^{2.67}$ . Figure 4f summarizes the variation of  $A_s$  with the spacing  $d$ . As seen,  $A_s$  reaches a maximum value of about 3.5 at  $d = 56$  nm. Such a spacing actually corresponds to the horizontal distance between the centers of adjacent skyrmions, at which the O1–O7 areas output almost synchronized signals, as shown in Fig. 4d. Note that unlike the common methods that use multiple synchronized oscillators to increase the power output<sup>2,6,8,13,14,67–71</sup>, our proposal involves only one oscillator with multiple oscillating units (i.e., skyrmions) and detection areas, which offers a potential way to obtain synchronized oscillation signals. It should be emphasized here that while two different oscillators can be synchronized (see Supplementary Fig. 8), our purpose is to use a single oscillator with a common skyrmion lattice to improve the output signal with a relatively high frequency. Although the skyrmion lattice is unstable at room temperature for the parameters used in this work, our proposal can be extended to synthetic ferrimagnetic systems with excellent thermal stability, as shown in Supplementary Fig. 10. Note that if there are ferromagnetic materials with skyrmion modes at THz frequencies<sup>72</sup>, exciting these modes may also produce high-frequency oscillating outputs.

In summary, we theoretically investigate a ferrimagnetic spin torque nano-oscillator leveraging a skyrmion lattice as its functional core. The weak Magnus force inherent to ferrimagnets enables oscillation frequencies up to 0.2 THz. Through micromagnetic simulations and analytical modeling via the Thiele equation, we comprehensively study the dependence of the skyrmion dynamics on system parameters. We further demonstrate the emergence of distinct, identical, and chaotic skyrmion trajectories

depending on the current injection area and damping. Finally, we propose a many-skyrmion oscillator configuration that significantly enhances the output power through synchronized signal detection. These results not only deepen our understanding of high-frequency skyrmion dynamics but also offer practical guidance for the design of next-generation THz spintronic oscillators.

## Methods

### Micromagnetic simulations

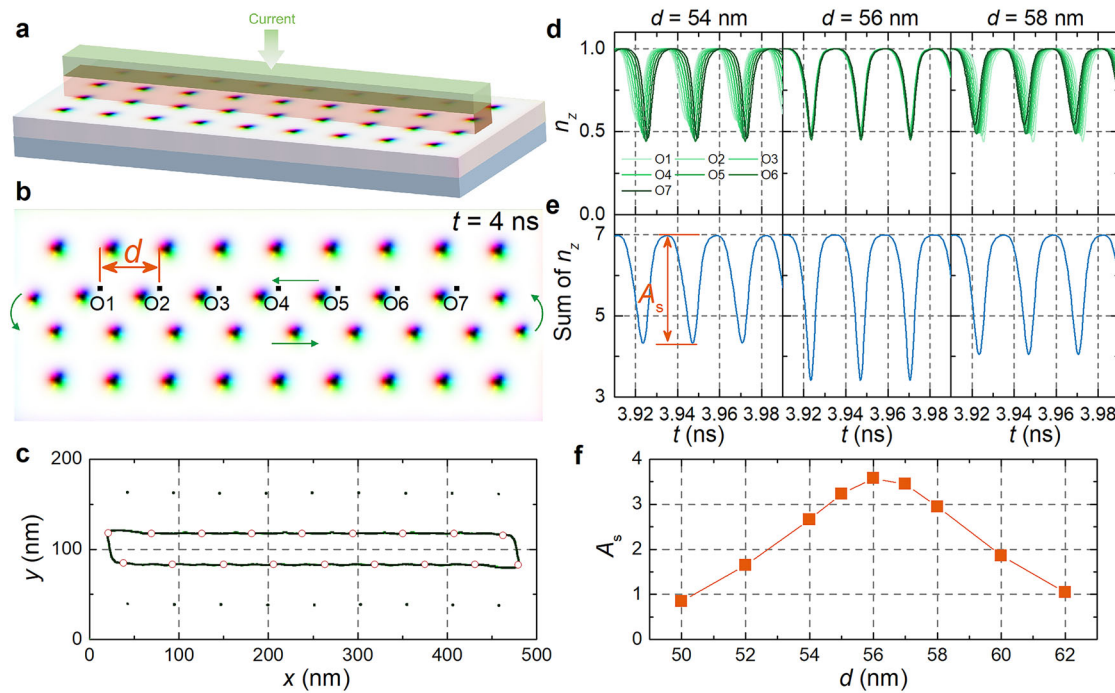
In this work, we consider a monolayer ferrimagnet whose sublattices have different magnetizations  $\mathbf{M}_1$  and  $\mathbf{M}_2$ . The simulations of ferrimagnetic skyrmion dynamics are carried out by using micromagnetic software MUMAX3<sup>50</sup> to numerically solve the equation of motion for the reduced magnetizations ( $\mathbf{m}_i = \mathbf{M}_i/M_{s,i}$  with the saturation magnetization  $M_{s,i}$ )

$$\dot{\mathbf{m}}_i = -\gamma_i \mathbf{m}_i \times \mathbf{H}_{\text{eff},i} + \alpha \mathbf{m}_i \times \dot{\mathbf{m}}_i + \gamma_i H_i (\mathbf{m}_i \times \mathbf{p}) \times \mathbf{m}_i, \quad (4)$$

where the subscript  $i = 1, 2$  is used to distinguish the two sublattices of ferrimagnet.  $\dot{\mathbf{m}}$  is the derivative of  $\mathbf{m}$  with respect to time.  $\gamma$  and  $\alpha$  denote the gyromagnetic ratio and the magnetic damping, respectively.  $\mathbf{H}_{\text{eff}}$  stands for the effective field, including the exchange field, the DMI field and the anisotropy field.  $\mathbf{p}$  represents the polarization vector and  $H_i = j\hbar P/(2\mu_0 e t_z M_{s,i})$  is the strength of dampinglike spin torque. Here  $j$  is the current density,  $\hbar$  the reduced Planck constant,  $P$  the spin polarization efficiency,  $\mu_0$  the vacuum permeability constant,  $e$  the elementary charge, and  $t_z$  the thickness of ferrimagnetic layer. The parameters used are provided in Supplementary Note 1.

### Expression of quantities in Thiele equation

The effective mass  $m_{\text{eff}} = \mu_0 t_z \rho^2 d_{xx}/(-4h_{\text{ex}})$  with  $\rho = M_{s1}/\gamma_1 + M_{s2}/\gamma_2$ ,  $d_{xx} = \int \partial_x \mathbf{n} \cdot \partial_x \mathbf{n} dx dy$  and  $h_{\text{ex}} = 2A_{\text{ex}}/(\mu_0 \Delta^2)$ . Here  $A_{\text{ex}}$  is the exchange coefficient



**Fig. 4 | Many-skyrmion oscillator.** **a** Geometry of the many-skyrmion oscillator using a strip-shaped current injector ( $460 \times 40 \text{ nm}^2$ ) placed on the ferrimagnet ( $500 \times 200 \text{ nm}^2$ ). **b** Magnetic structure at simulation time  $t = 4 \text{ ns}$ . Seven black squares (labeled O1–O7) with equal spacing  $d$  and the same size  $5 \times 5 \text{ nm}^2$  indicate

the output areas. The green arrows describe the rotation direction of the skyrmions. **c** Skyrmion trajectories. **d** The  $z$ -component  $n_z$  of the Néel vector in the regions O1–O7 and **e** the sum of  $n_z$  of all output regions, with different spacings  $d$ . **f** Amplitude  $A_s$  of the sum of  $n_z$  with different values of  $d$ .

and  $\Delta$  is the cell size. The gyrovectore  $\mathbf{G} = 4\pi Q\mu_0 t_z (M_{s1}/\gamma_1 - M_{s2}/\gamma_2) \mathbf{e}_z$  with the topological charge  $Q$ . The frictional force  $\mathbf{F}_\alpha = -\alpha \mathbf{L} \dot{\mathbf{r}}_c = -\alpha (\mu_0 t_z d_{xx} \rho) \dot{\mathbf{r}}_c$ . The skyrmion-skyrmion interaction force,  $\mathbf{F}_{ss} = -\nabla U_{ss}$  is given by the interaction potential  $U_{ss}$ .

## Data availability

The data supporting the findings of this study are available within this article and its Supplementary Information. Additional data that support the findings of this study are available from the corresponding author on reasonable requests. The micromagnetic simulation software MUMAX3 used in this work is open-source and can be accessed freely at <http://mumax.github.io/>.

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## Author contributions

Y.Z. coordinated the project. L.S. performed the micromagnetic simulations and the theoretical analysis. L.S. drafted the manuscript and revised it with input from Q.S., J.Å., and Y.Z. All authors discussed the results and reviewed the manuscript.

## Competing interests

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## Additional information

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**Correspondence** and requests for materials should be addressed to Yan Zhou.

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